



Part 1: Polyethylene Pressure Pipes Design for Dynamic Stresses

INTRODUCTION

Polyethylene pressure pipes are designed on the basis of a burst regression line for pipes subjected to constant internal pressure. From this long-term testing and analysis, nominal working pressure classes are allocated to pipes as a first indication of the duty for which they are suitable. However, there are many other factors which must be considered, including the effects of dynamic loading. Whilst most gravity pressure lines operate substantially under constant pressure, pumped lines frequently do not and it is essential that the effects of this type of loading be considered in the pipeline design phase to avoid premature failure. This note is intended to assist in the selection of pipe class for polyethylene pipes in applications involving transient and cyclic operating pressures.

Pressure fluctuations in pumped mains result from events such as pump start-up and shutdown or valves opening and closing. The approach adopted for pipe design and class selection when considering these events depends on the anticipated frequency of the pressure fluctuation as follows:

- for random, isolated surge events, for example, those which result from emergency shutdowns, the designer must ensure that the maximum and minimum pressures experienced by the system are within acceptable limits; and
- for frequent, repetitive pressure variations, the designer must consider the potential for fatigue and design accordingly.

DEFINITIONS

For the purposes of this note, surge is defined as a rapid, very short-term pressure variation caused by an accidental, unplanned event such as an emergency shutdown resulting from a power failure. Surge events are characterised by high pressure rise rates with no time spent at the peak pressure. The maximum duration of a surge event is about 5 minutes.

Fatigue is associated with a large number of repetitive events. The key factors to consider are the size and frequency of the repeated event. For large pressure cycles, a lower number of events can be tolerated in the pipe lifetime. For smaller pressure changes, a greater number of events is acceptable.

The gradual diurnal pressure changes which occur in most distribution pipelines as a result of demand variation will not cause fatigue. The only design consideration required for this type of pressure fluctuation is that the maximum pressure should not exceed the pressure rating of the pipe.

SURGE DESIGN

It has long been recognised that polyethylene pipes are capable of handling short-term stresses far greater than the long-term loads upon which they are designed. However, this characteristic feature has, to date, not been utilised in design in Australia. Previous design recommendations have advised that the peak pressure should not exceed the nominal working pressure of the pipe.

Recently, studies in the UK (1) have examined the response of plastics pipes to short-term over-pressurisation. This work has culminated in the publication of a design recommendation (2) allowing significant over-pressurisation of plastics pipes during rapid surge events. However, while these results highlight the capabilities of plastics pipes in this respect, they do not discuss the effect of over-

pressurisation on the pipe where it is restrained by tapping bands or flange connections. The effect on other pipeline components is also not considered.

Field tests of installed pipelines are conducted to verify the pipeline design and construction. These tests are generally carried out at a pressure of 1.25 times the maximum system operating pressure. Since the test pressure is generally the highest pressure a pipeline will experience, the field test serves to demonstrate that all system components, including items such as anchor blocks which are formed in-situ, will be satisfactory for the operating conditions.

The demonstrated ability of polyethylene pipes to accommodate short-term surge pressures can be utilised to advantage by allowing some over-pressurisation. However, it is recommended that the peak design pressure is limited to the field test pressure of that pipeline in order to ensure that the pipeline as a whole is capable of performing under these conditions.

Where the generation of negative pressures is anticipated, the possibility of transverse buckling should be considered. This topic is well covered in other technical literature.

FATIGUE DESIGN

Many materials will fail at a lower stress when subjected to cyclic or repetitive loads than when under static loads. This type of failure is known as fatigue. For thermoplastics pipe materials, fatigue is only relevant where a large number of stress cycles are anticipated. The important factors to consider are the magnitude of the stress fluctuation and the loading frequency. Where large stress fluctuations are predicted, fatigue design may be required where the total number of cycles in the operational lifetime of the pipe exceeds 100,000. For smaller stress cycles, a larger number of cycles can be tolerated.

The fatigue response of thermoplastics pipe materials has been extensively investigated (3-9). The results of laboratory studies can be used to establish a relationship between stress range, defined here as the difference between the maximum and minimum stress (see Fig 2), and the number of cycles to failure. From these relationships it is possible to derive load factors that can be applied to the operating pressures, to enable selection of an appropriate class of pipe.

This type of experimental data inevitably has a degree of scatter and it has been Australian practice, after Joseph (3), to adopt the lower bound for design purposes. This approach is retained here because it ensures the design has a positive safety factor and recognises that pipelines may sustain minor surface damage during installation, which could promote fatigue crack initiation. Note that for fatigue loading situations, the maximum pressure reached in the repetitive cycle should not exceed the static pressure rating of the pipe.

Table 1 gives the recommended fatigue load factors for thermoplastics pipes. This is also graphically presented in Figure 1.

Table 1

TOTAL CYCLES	APPROX. NO CYLCES/DAY FOR 100 YR LIFE	FATIGUE LOAD FACTORS PE80B AND PE100
36,500	1	1.00*
100,000	3	1.00
300,000	8	1.00
500,000	14	0.95
1,000,000	27	0.88
5,000,000	137	0.74
10,000,000	274	0.68
50,000,000	1370	0.57

Note: *Maximum allowable factor for fatigue loading pressure cycles

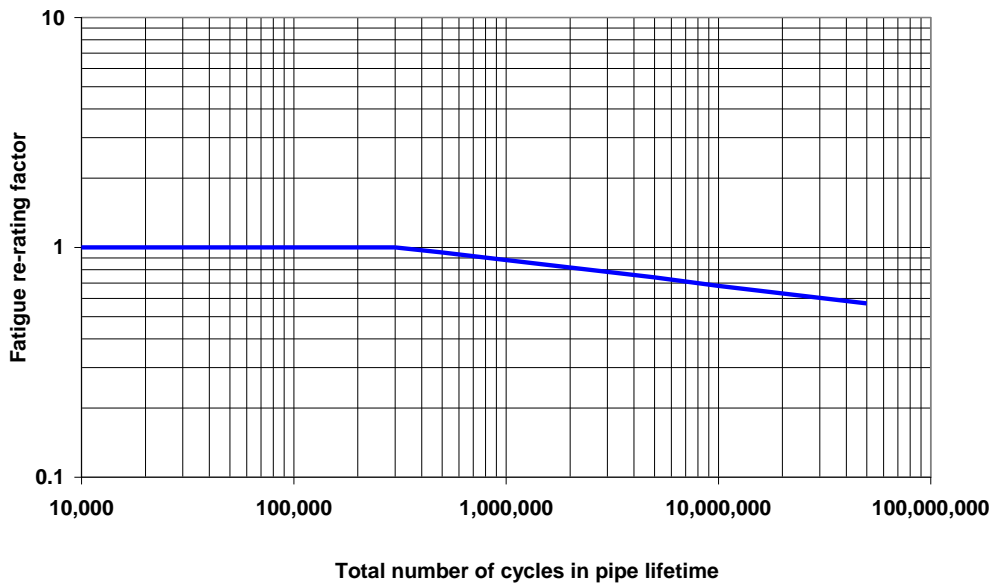


FIGURE 1 – FATIGUE LOAD FACTORS FOR POLYETHYLENE PIPES

PROCEDURE

To select the appropriate pipe class for fatigue loading, the following procedure should be adopted:

1. Estimate the likely pressure range, ΔP , i.e., the maximum pressure minus the minimum pressure.
2. Estimate the frequency or the number of cycles per day which are expected to occur.
3. Determine the required service life and calculate the total number of cycles which will occur in the pipe lifetime.
4. Using Table 1 or Figure 1, look up the fatigue load factor for the appropriate pipeline material and number of cycles.
5. Divide the pressure range by the fatigue load factor to obtain an equivalent operating pressure.
6. Use the equivalent operating pressure to determine the class of pipe required.

DEFINITION OF PRESSURE RANGE

For simplicity, the pressure range is defined as the maximum pressure minus the minimum pressure, including all transients, experienced by the system during normal operations as shown in Figure 2. The effect of accidental conditions such as power failure may be excluded.

Figure 2 also illustrates the definition of a cycle as a repetitive event. In some cases, the cycle pattern will be complex, and it may be necessary to also consider the contribution of secondary cycles.

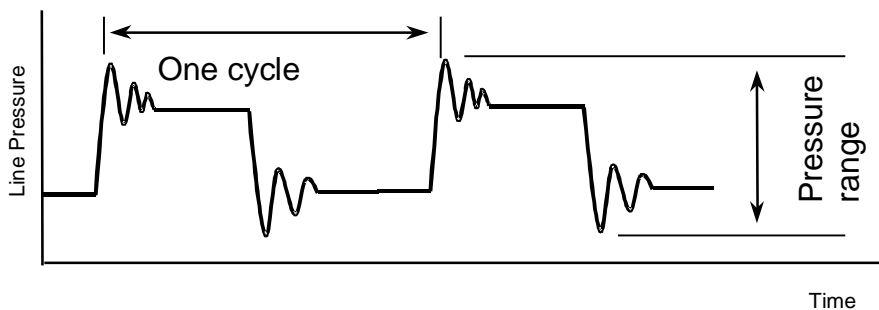


FIGURE 2 – PRESSURE CYCLE

COMPLEX CYCLE PATTERNS

Pumping systems are frequently subject to surging following the primary pressure transient on switching. Such pressure surging decays exponentially, and in effect, the system is subjected to a number of minor pressure cycles of reducing magnitude. In order to take this into account, the effect of each minor cycle is related to the primary cycle in terms of the number of cycles which would produce the same crack growth as one primary cycle.

Using this technique, it is shown in Reference (3) that a typical exponentially decaying surge regime is equivalent to 2 primary cycles. Thus, for design purposes, the primary cycle amplitude only is considered, with the frequency doubled.

In general, similar technique may be applied to any situation where smaller cycles exist in addition to the primary cycle. Empirically crack growth is related to stress range according to $(\Delta\sigma)^{3.2}$. Thus, n secondary cycles of magnitude $\Delta\sigma_1$ may be deemed equivalent in effect to one primary cycle,

Where:

$$n = \left(\frac{\Delta\sigma_0}{\Delta\sigma_1} \right)^{3.2}$$

For example, a secondary cycle of half the magnitude of the primary cycle:

$$n = \left(\frac{2}{1} \right)^{3.2} = 9.2$$

So it would require 9 secondary cycles to produce the same effect as one primary cycle. If they are occurring at the same frequency, the effective frequency of primary cycling is increased by 1.1 for the purpose of design.

EXAMPLE

A sewer rising main has a pump pressure, including static lift and friction losses, of 600 kPa. When the pump starts up, the pressure rises rapidly to 1.1 MPa before decaying exponentially to the static pumping pressure. On pump shut down, the minimum pressure experienced by the system is 100 kPa. On average, the pump will start up 27 times per day. A minimum life of 100 years is required.

The maximum pressure experienced indicates that a minimum class of PN12.5 will be required. A fatigue analysis is now needed in order to determine suitability or otherwise of PN12.5.

In this system, the pressure range is 1MPa. The pump will start up approximately 1,000,000 times in a 100-year lifetime. However, the exponential cycle pattern means that this should be doubled for design purposes. Therefore, the system should be designed to withstand approximately 2,000,000 cycles in a 100-year lifetime.

Using Figure 1 to determine the fatigue load factors for polyethylene pipes at 2×10^6 cycles gives the following class selections:

MATERIAL	LOAD FACTOR (FIGURE 1)	EQUIV. OPERATING PRESSURE (MPa)	MINIMUM PIPE CLASS SELECTION
PE80B or PE100	0.8	1.0/0.8=1.25	PN12.5

The fatigue analysis thus determines that PN12.5 is suitable for PE 80B and PE 100.

EFFECT ON TEMPERATURE

Few data have been established concerning the relationships between fatigue performance and temperature. Reference 3 suggests that effects are marginal if any within the range of normal pipeline operating temperatures. It might be expected that higher temperatures could actually inhibit fatigue crack growth by blunting of the crack tip through the reduced yield strength.

Normal temperature de-rating principles should apply in class selection for maximum operating pressure. Fatigue should then be considered separately, and the highest-pressure class selected.

That is select the highest class arrived via:

- a) Static design including temperature derating; or
- b) Dynamic design as covered herein.

SAFETY FACTORS

The fatigue design guidelines presented in Table 1 are based on the lower bound of laboratory test data. They are therefore considered conservative and no additional safety factor need be applied in general. However, where the magnitude or frequency of dynamic stresses cannot be estimated in design with any reasonable degree of accuracy, appropriate caution should obviously be applied. This judgement is in the hands of the designer.

Whilst it is always possible to predict the steady operating conditions with good accuracy, it will occasionally be the case, in complex systems, that is impossible to predict the extent of surge pressures. In such circumstances, relatively low-cost surge mitigation techniques, for example solid state soft-start motor controllers, should be considered. It is of course recommended that actual operating conditions for all systems should be measured, as a matter of routine, when the system is commissioned. Should surge pressure amplitudes in the event exceed expected levels, it is relatively easy matter to retrofit control equipment to ensure that they are kept in check.

DESIGN HINTS

To reduce the effect of dynamic fatigue in an installation, the designer can:

Limit the number of cycles by:

- Increasing well capacity for a sewer pumping station;
- Matching pump performance to tank size to eliminate short demand cycles for an automatic pressure unit; or
- Using double-acting float valves or limiting starts on the pump by the use of a time clock when filling a reservoir.

Reduce the dynamic range by:

- Eliminating excessive water hammer; or
- Using a larger bore pipe to reduce friction losses.

FITTINGS

With respect to surge and fatigue, fittings performance is dependent upon several factors, and PIPA has provided *PART 2 FUSION FITTINGS FOR USE WITH POLYETHYLENE PRESSURE PIPES DESIGN FOR DYNAMIC STRESSES* in document POP010B.

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